

# A Multiband LTE SAW-less CMOS Transmitter with Source-Follower-Driven Passive Mixers, Envelope-Tracked RF- PGAs, and Marchand Balun

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# Outline

- Background
- Transmitter architecture
- Circuit topologies:
  - Quadrature modulator (QMOD)
  - RF programmable gain amplifier (RF-PGA)
  - Balun
- Measurement results
- Summary



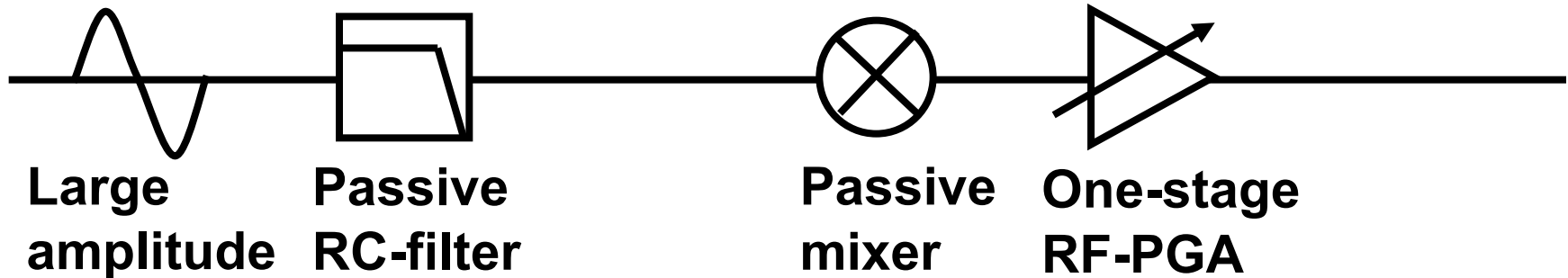
# Background

- Long Term Evolution (LTE):
  - Higher data transfer rate ( $>10$  Mbps) than W-CDMA and HSPA
  - Higher PAPR signals and more frequency bands
  - ➔ High linearity ( $ACLR < -42$  dBc) and multi-band operation (700 MHz – 2.6 GHz)
- SAW-less operation desired for low cost
  - ➔ Low RX-band noise ( $< -158$  dBc/Hz)

PAPR: Peak-to-average power ratio, SAW: Surface Acoustic Wave,  
ACLR: Adjacent channel leakage ratio,



# Approach

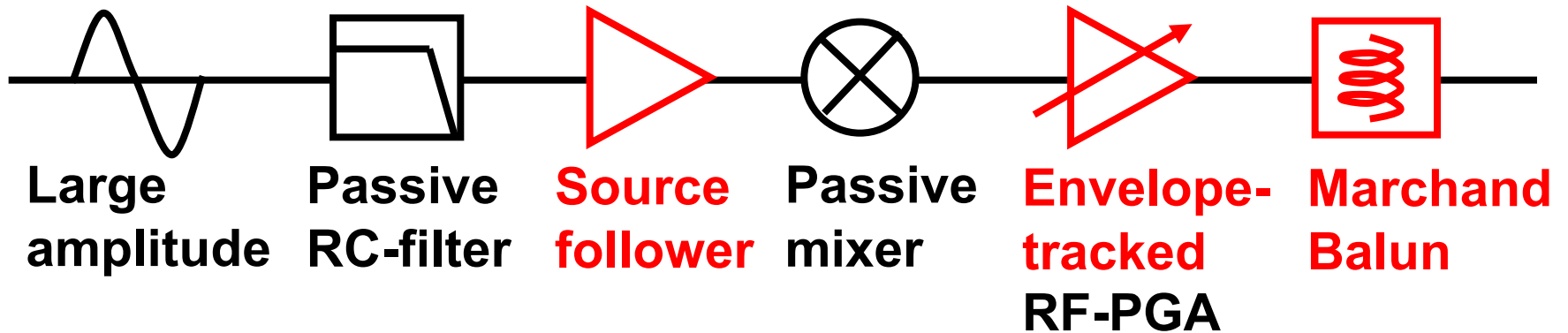


## For low noise

- Large amplitude base-band signal
- Passive RC-filter
- Passive mixer
- One-stage RF-PGA



# Approach



## For low noise

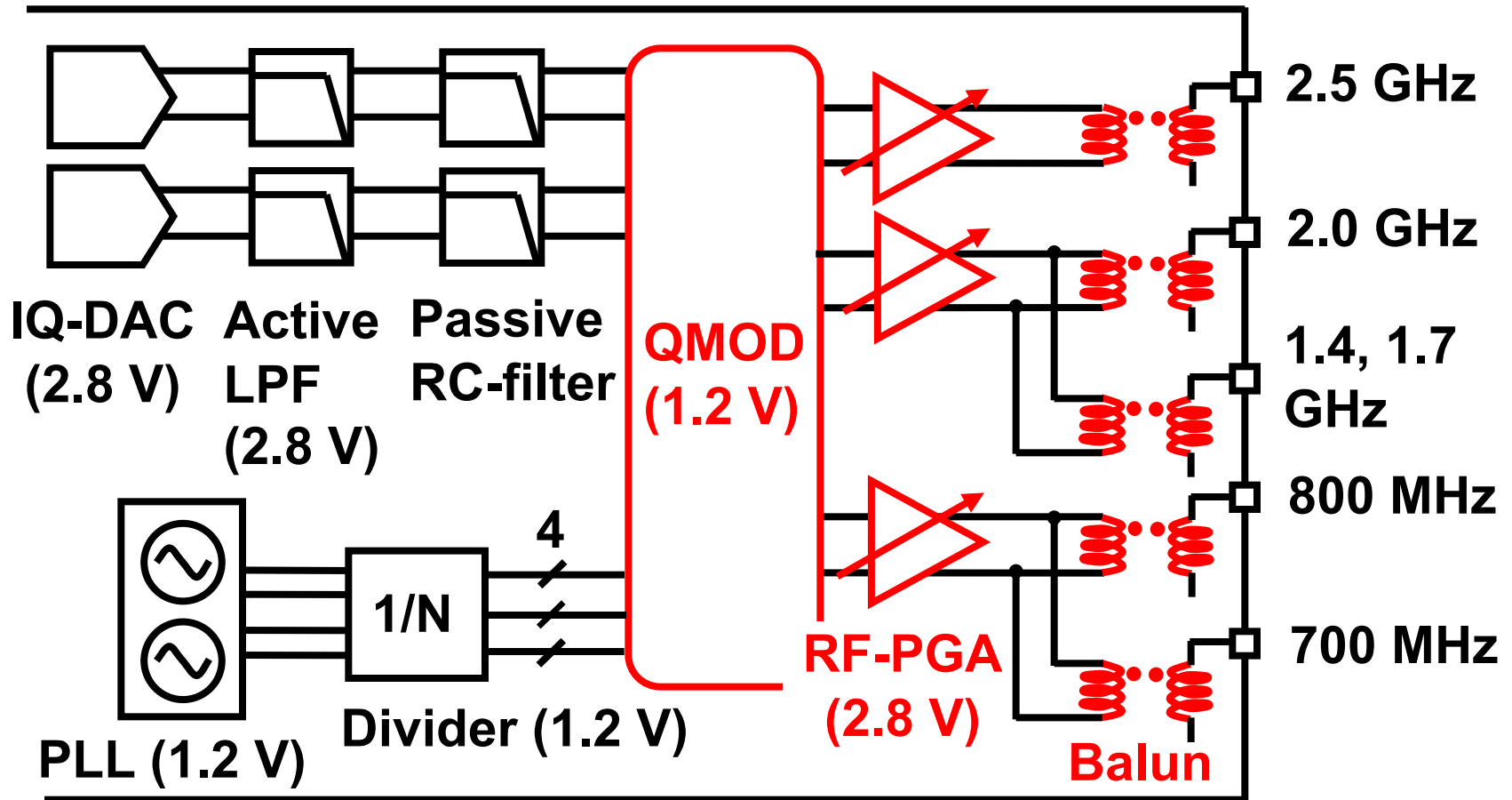
- Large amplitude base-band signal
- Passive RC-filter
- Passive mixer
- One-stage RF-PGA

## New topologies

- Source-follower-driven passive mixer
- Envelope-tracked RF-PGA
- Marchand balun



# Block Diagram of Transmitter

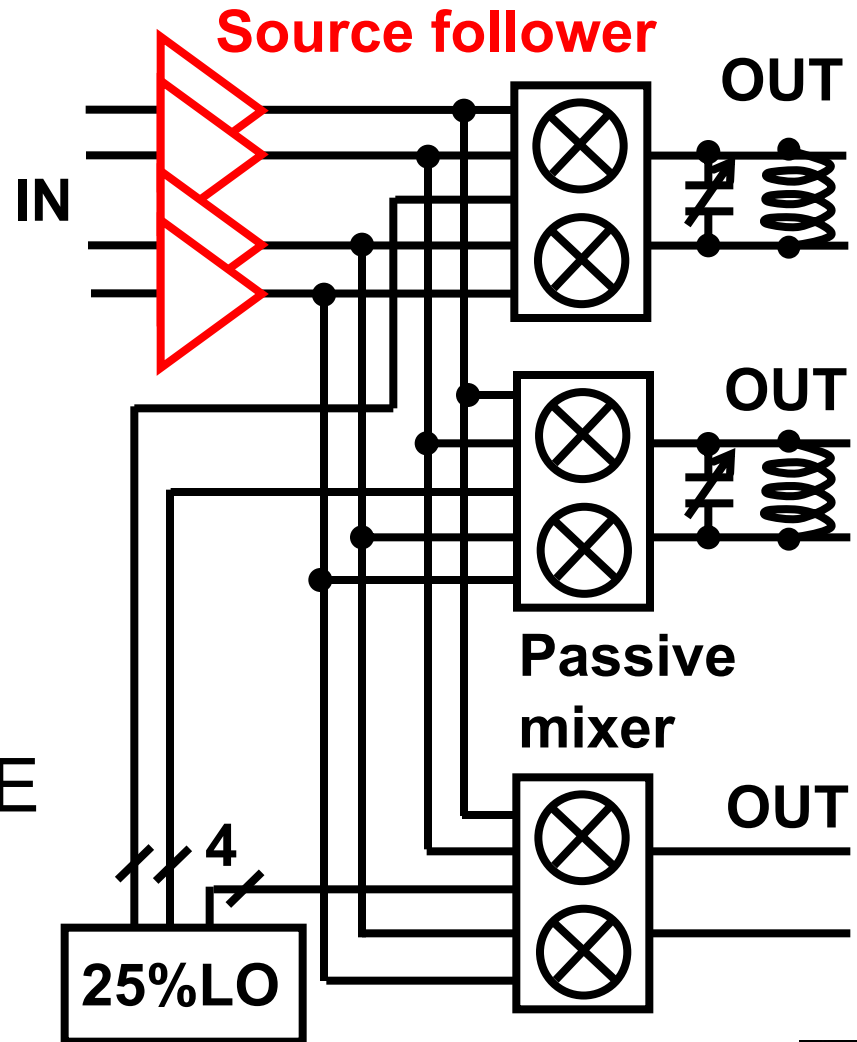


- IQ direct conversion architecture
- **New topologies: QMOD, RF-PGA, and balun**



# Quadrature Modulator

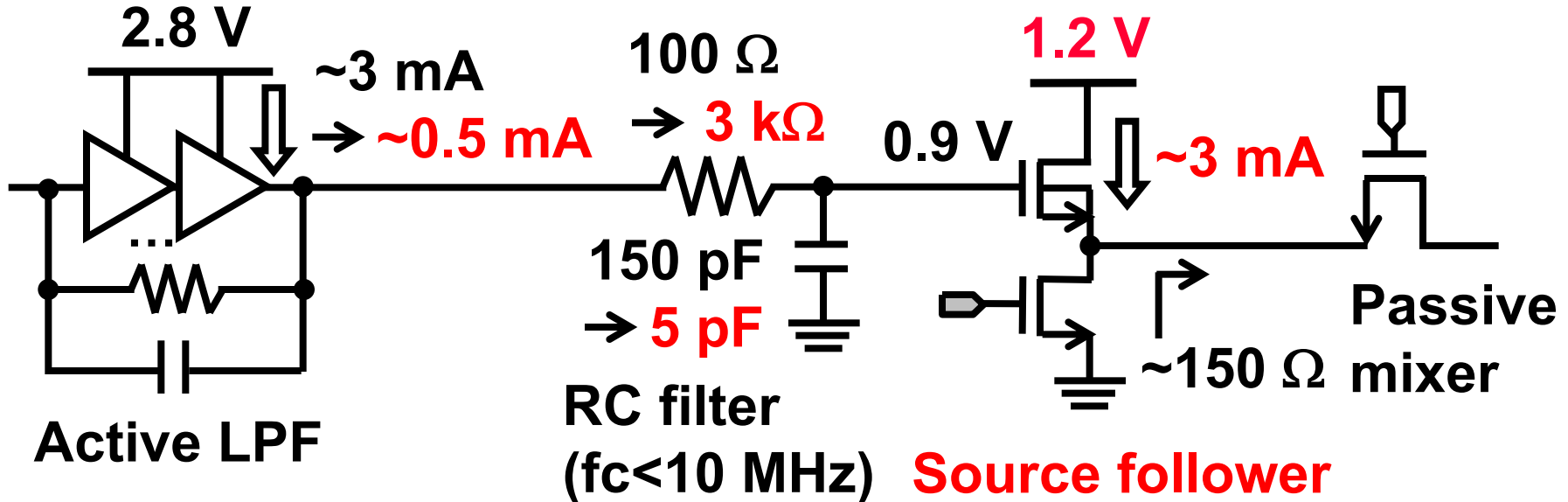
- Circuit topology:
  - Source follower
  - Passive mixer
  - 25%-duty-cycle LO
- Performance:
  - $-163$  dBc/Hz noise
  - $-48$  dBc ACLR for LTE
  - $17.5$  mA from  $1.2$  V (Band 1)



Source followers are used as driver for passive mixers



# Advantages of Source Follower



- Advantages:

- Small power consumption to drive mixer  
(~3 mA from 2.8 V  $\rightarrow$  1.2 V, -13 mW)
- Small capacitor for RC-filter  
(150 pF  $\rightarrow$  5 pF, -0.2 mm<sup>2</sup>)

**➔ Low-power and small-area transmitter**

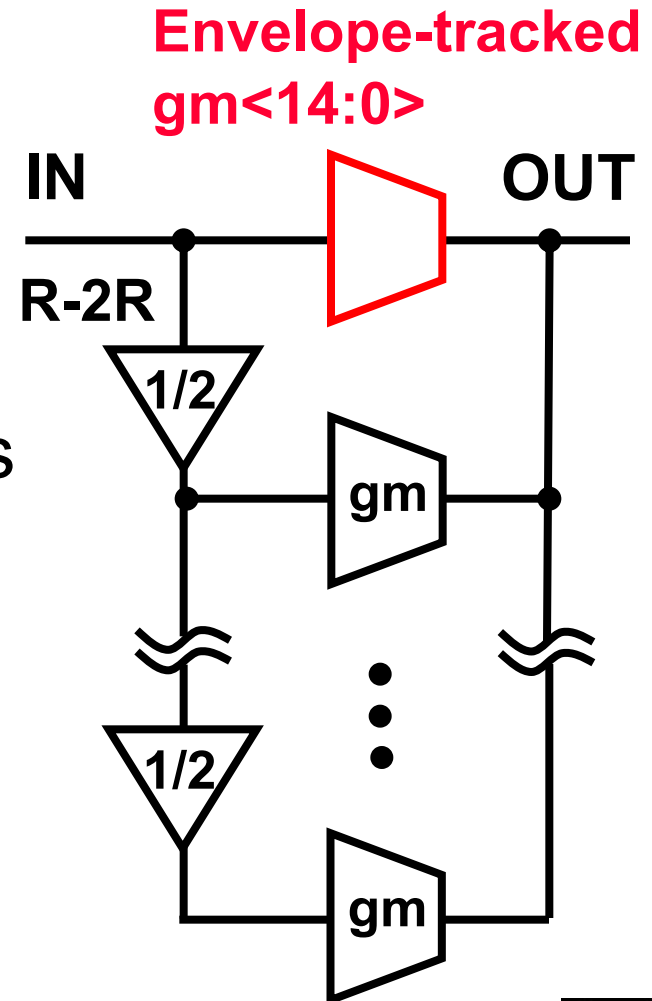




# Envelope-Tracked RF-PGA

- Circuit topology:
  - 15 thermometer-weighted transconductors
  - 14 binary-weighted transconductors with R-2R ladders
- Performance:
  - 74 dB gain control range
  - 32 mA for 3 dBm output power (Band 1)

Envelope-tracked biasing is employed on transconductors

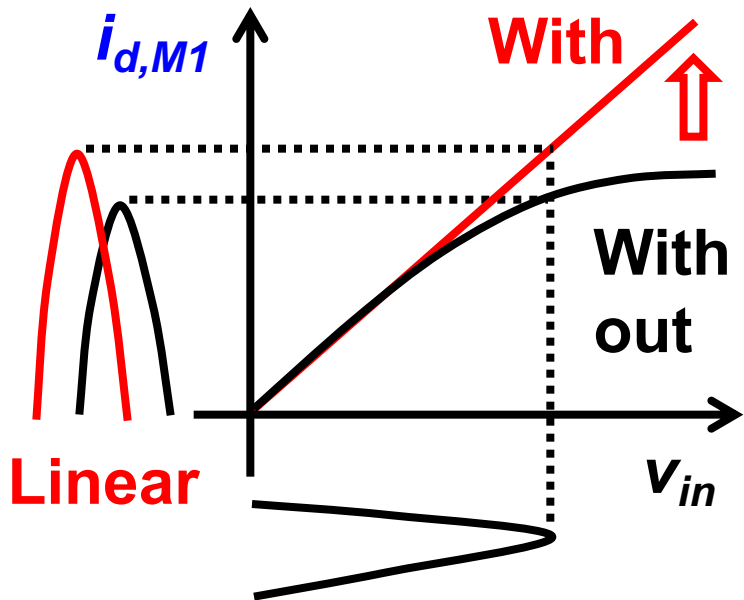
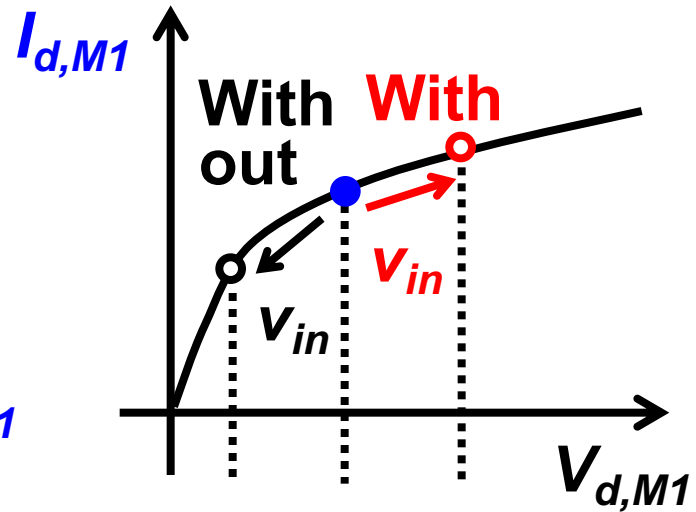
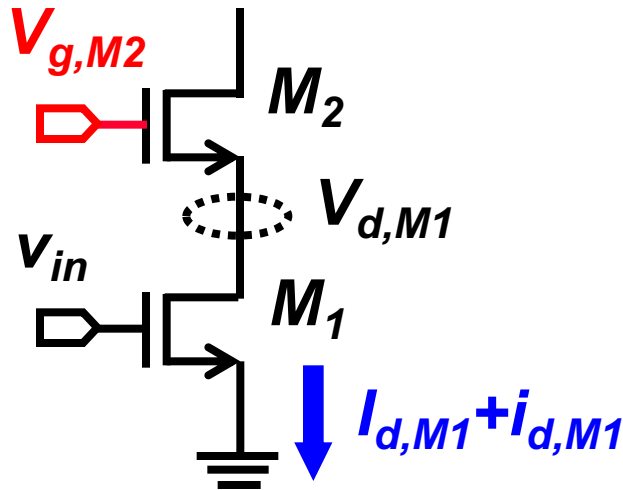


Ref. VLSI 2010,  
Renesas



# Envelope-Tracked Biasing

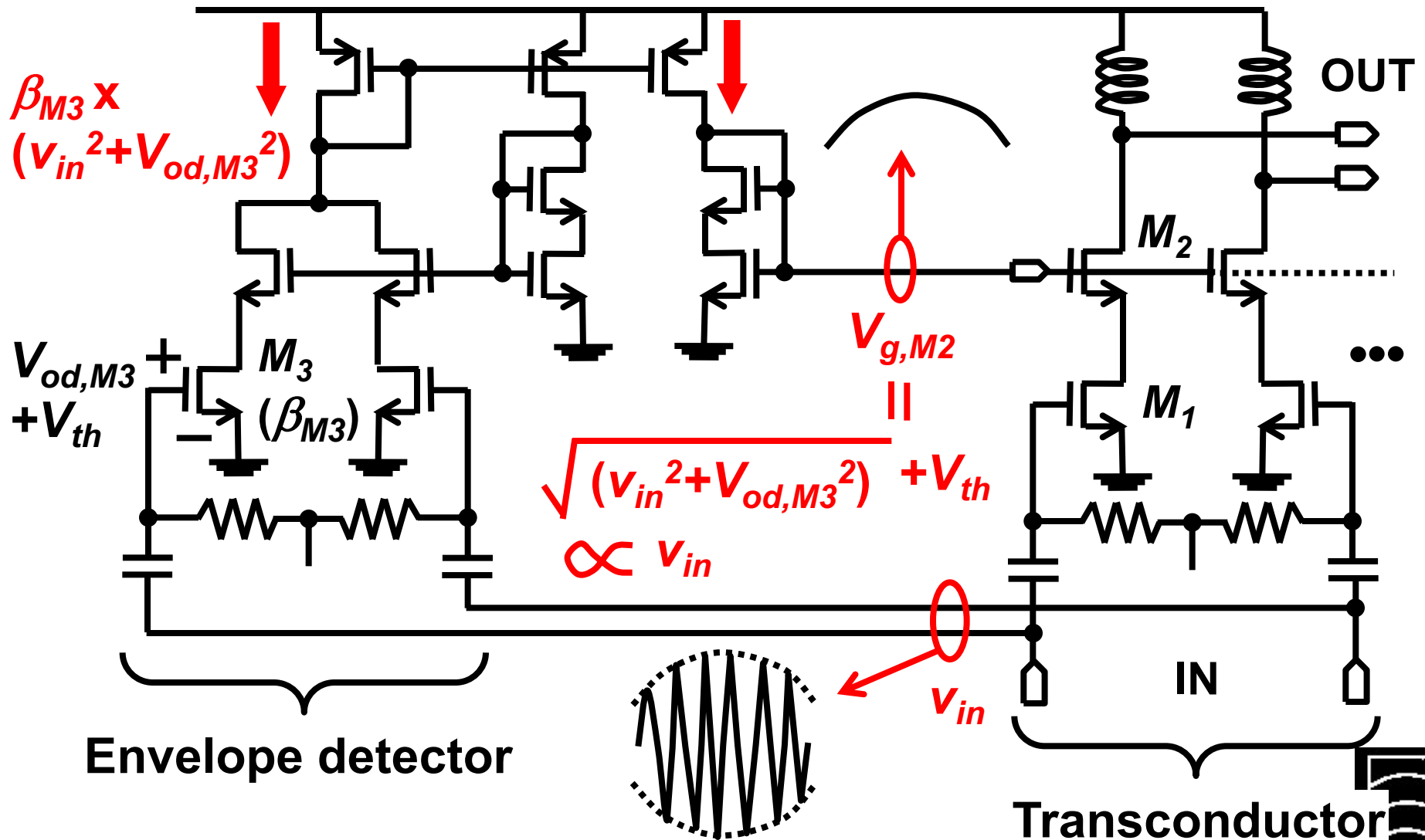
With  
Without



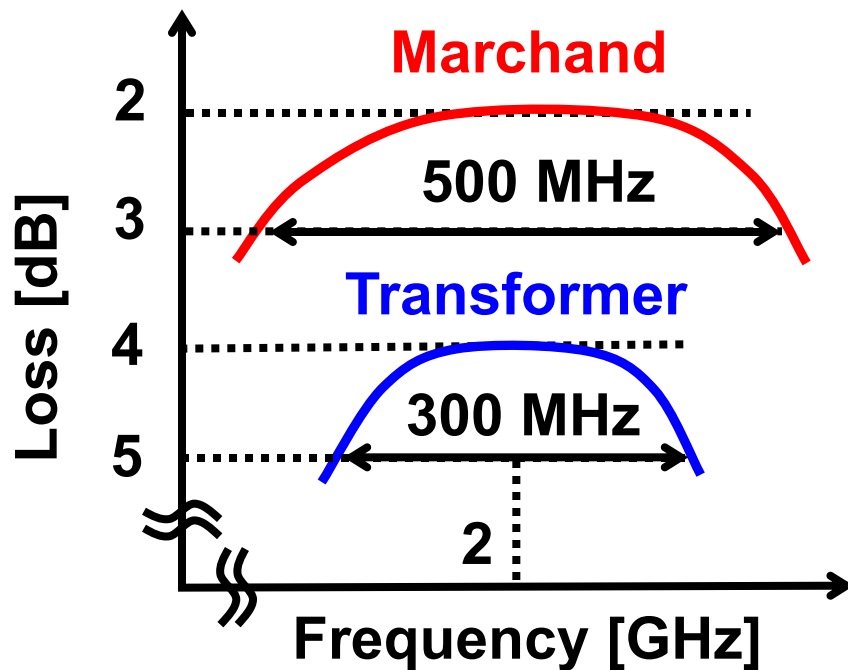
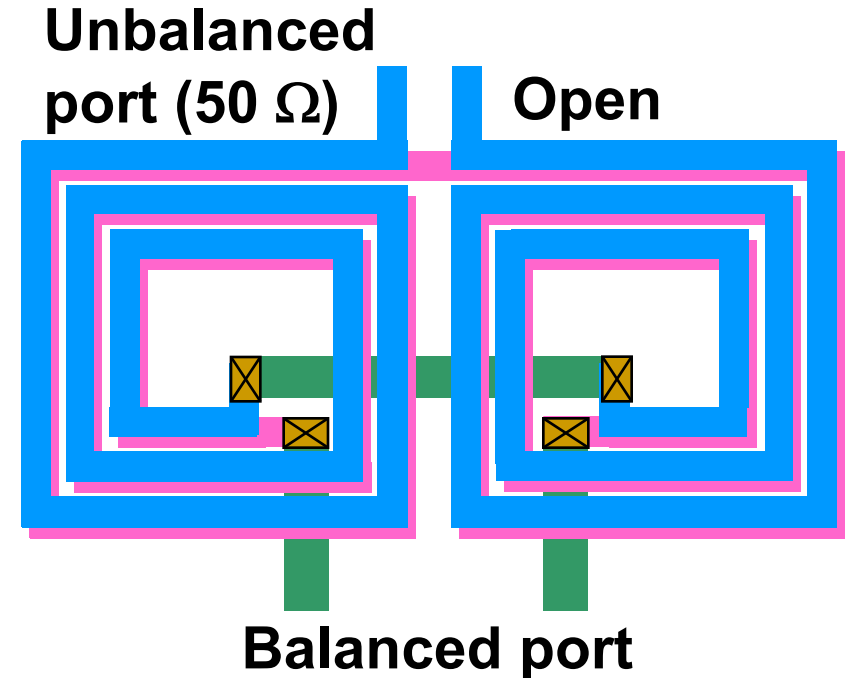
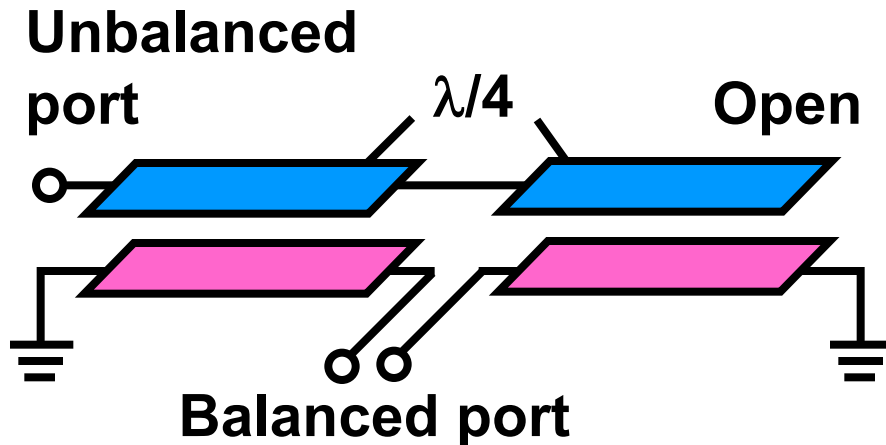
$V_{g,M2}$  tracks to envelope signal and the linearity of transconductor improves (OCP1dB=11 dBm  $\rightarrow$  14 dBm)



# Envelope-Tracked Biasing Circuit



# Marchand Balun

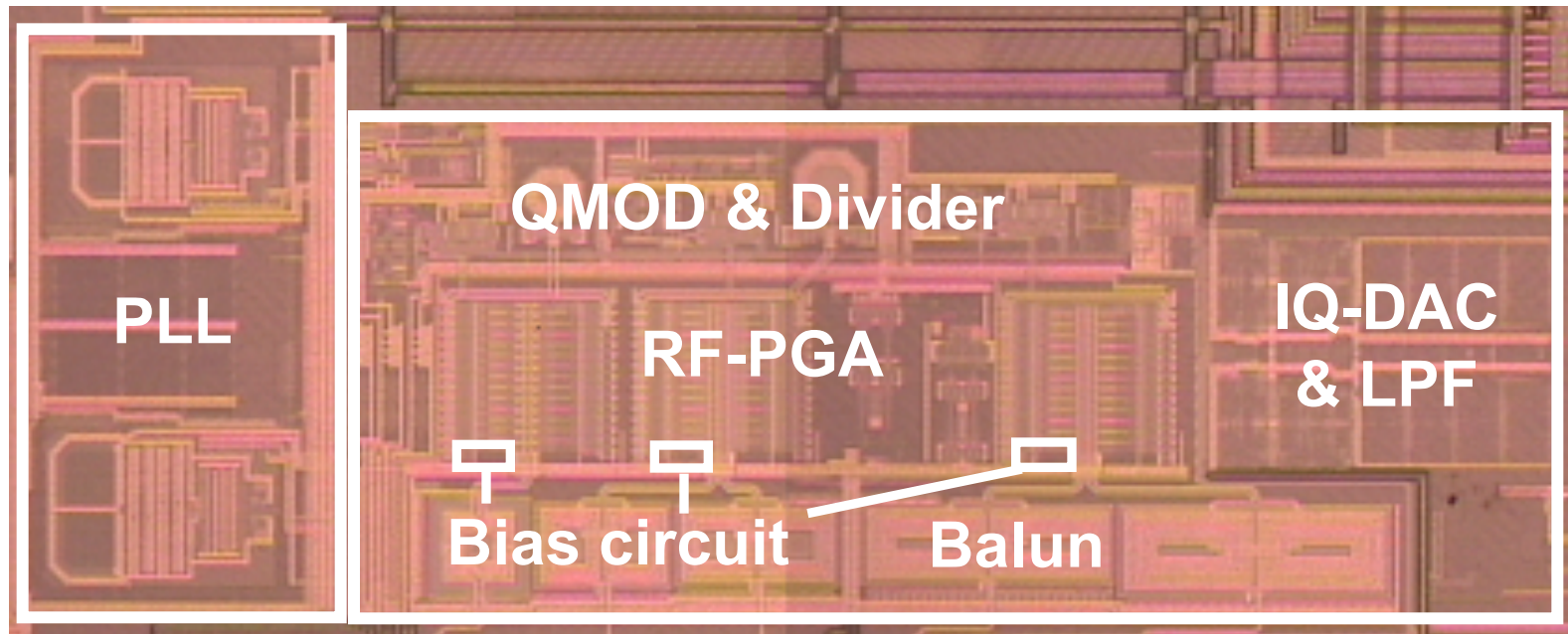


Marchand balun provides:

- Less loss ( $\sim 2$  dB)
- Broader 1-dB bandwidth ( $\sim 500$  MHz)



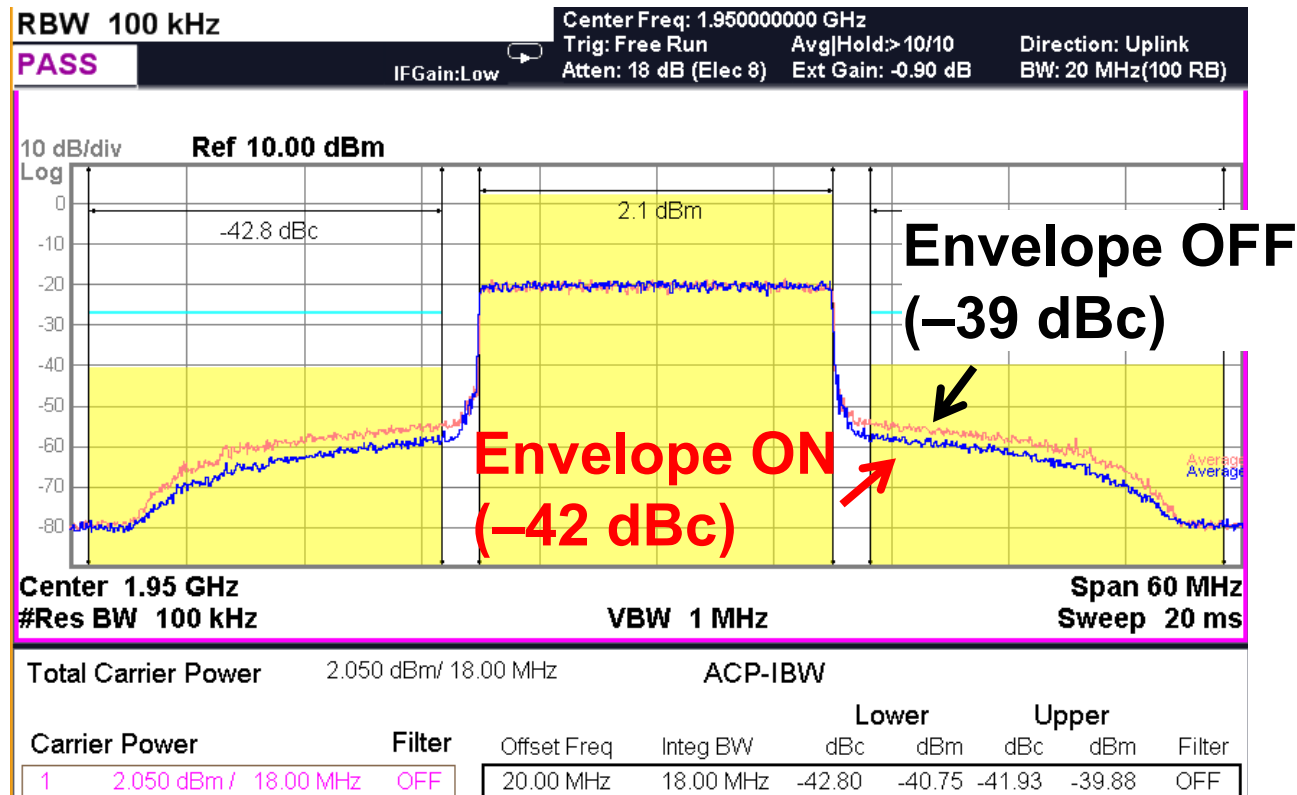
# Microphotograph



- 65-nm CMOS technology
- Chip area: 4.5 mm<sup>2</sup>
- Ball grid array (BGA) package



# Output Spectrum for LTE Signal



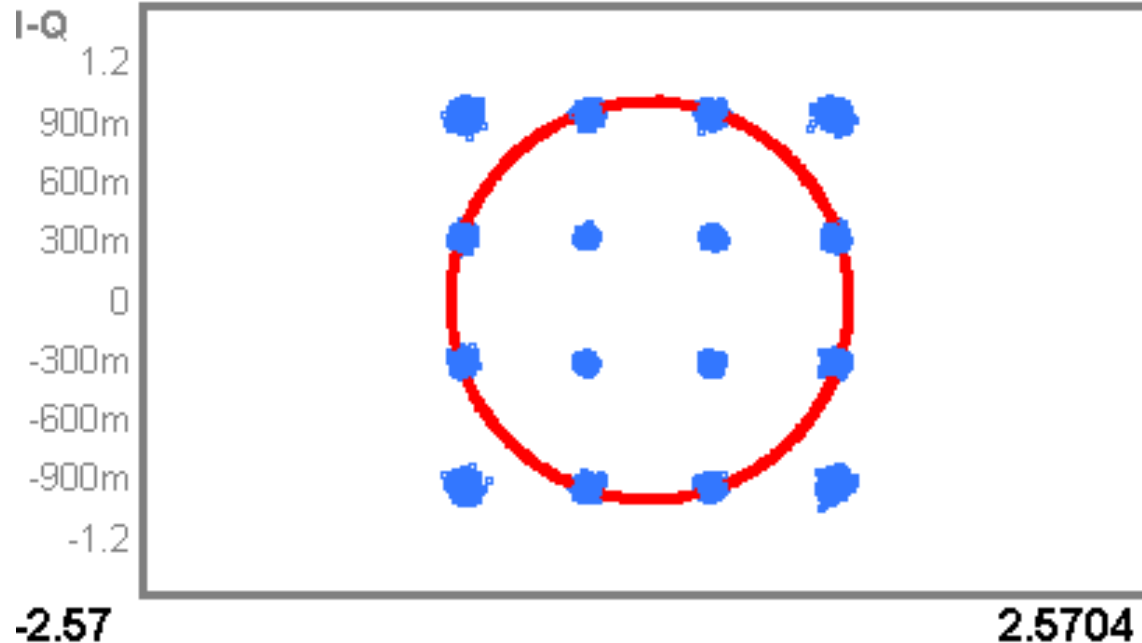
- LTE signal: 16 QAM and 20 MHz bandwidth
- Band 1 (1.95 GHz) and 2 dBm output power
- **ACLR=-42 dBc (Envelope ON), -39 dBc (Envelope OFF)**



# EVM for LTE Signal

Ch1 OFDM Meas

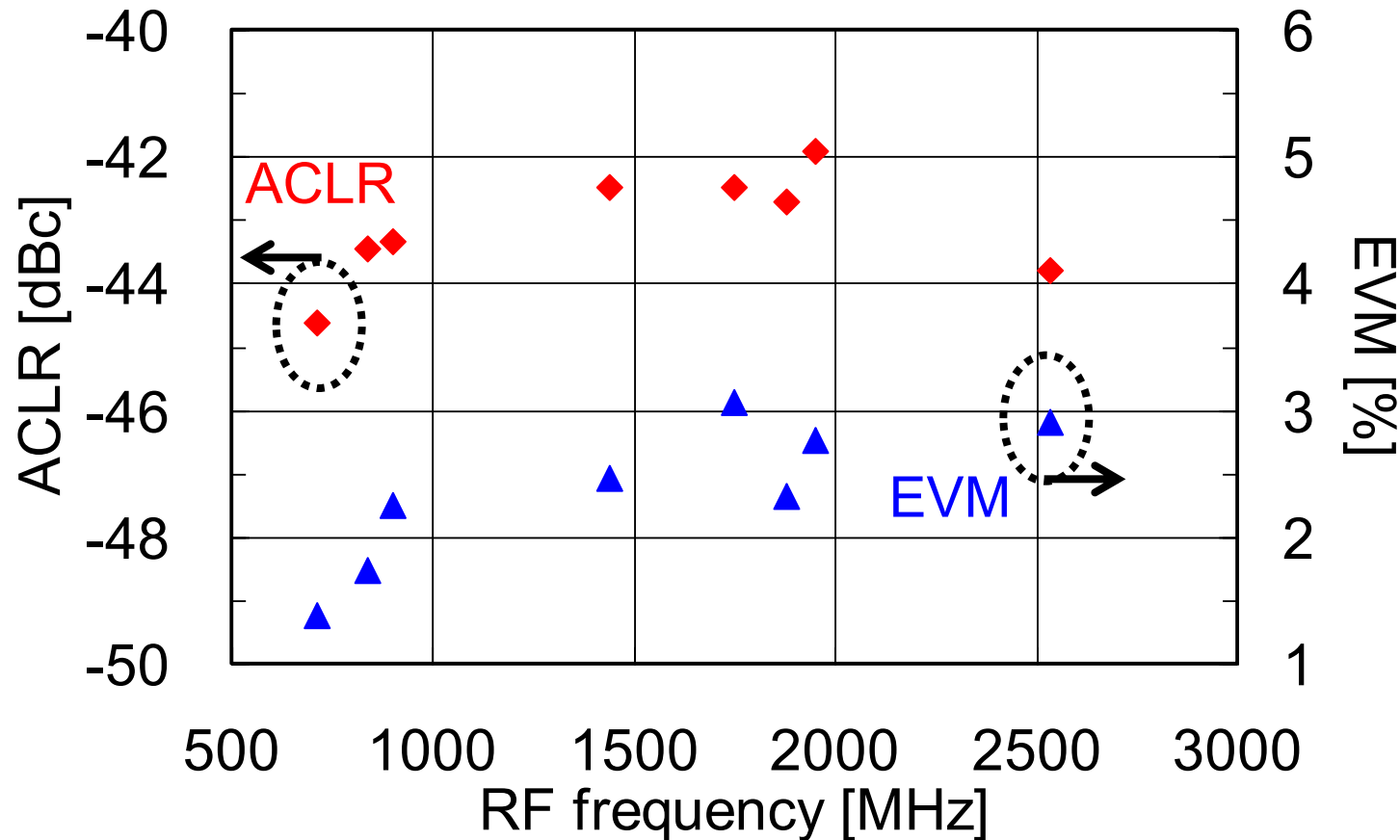
300 m/div Ref0



- LTE signal: 16 QAM and 20 MHz bandwidth
- Band 1 (1.95 GHz) and 2.1 dBm output power
- **EVM=2.8% (Envelope ON)**



# Measured ACLR and EVM



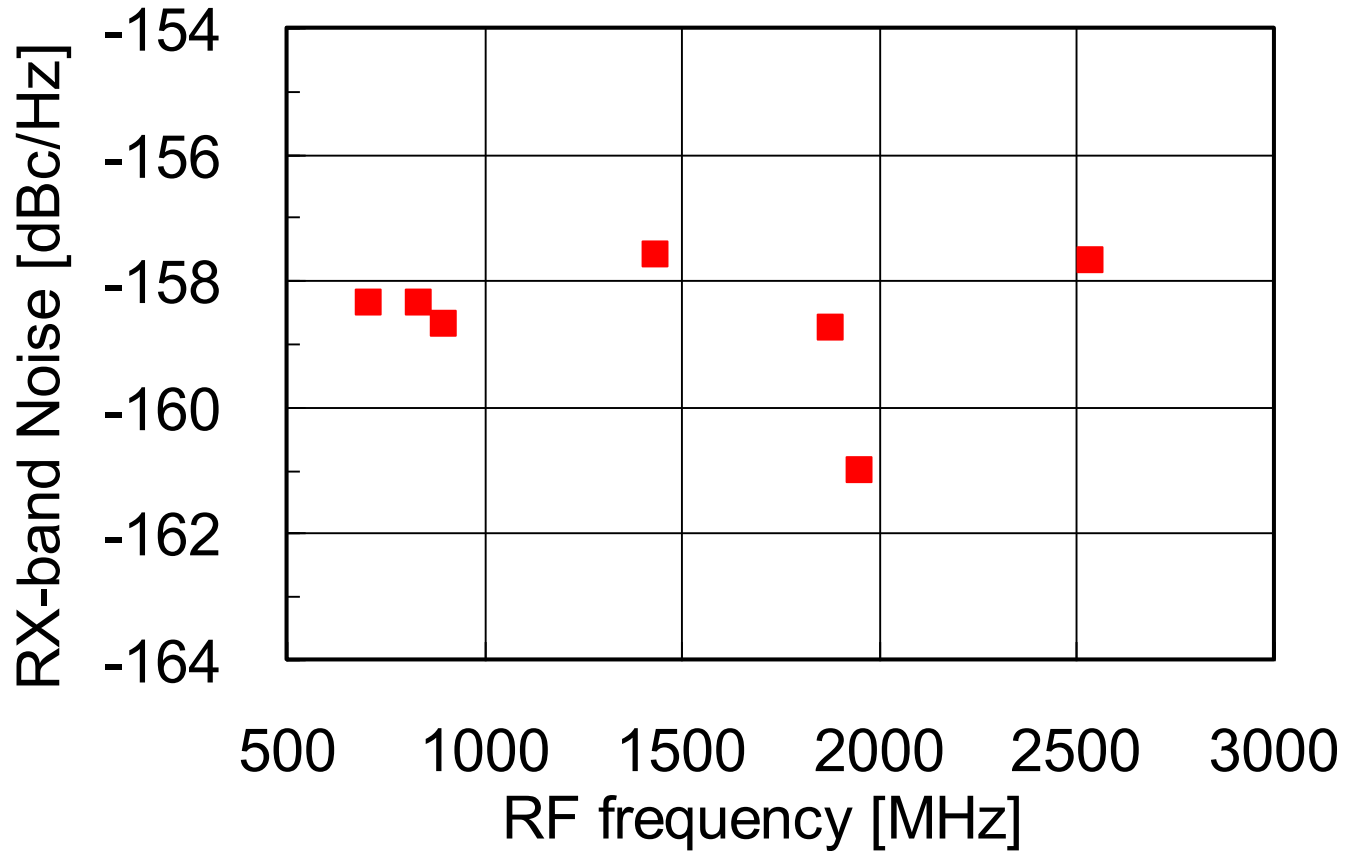
From 700 MHz to 2.6 GHz,

- **ACLR < -42 dBc** (3GPP ACLR spec. < -30 dBc)
- **EVM < 3%** (3GPP EVM spec. < 12.5%)





# Measured RX-band Noise



From 700 MHz to 2.6 GHz,

- RX-band noise  $\leq -158$  dBc/Hz



# Performance Comparison for Band 1

Performance	This work	IMEC / Renesas* (ISSCC 2011)
Pout [dBm]	2.1	1.7
ACLR [dBc]	-42	-39
EVM [%]	2.8	2.5
RX-band noise [dBc/Hz]	-161	-160
Current [mA]	27/44 (1.2 V/2.8 V)	25/40 (1.1 V/2.5 V)

\*: Without IQ-DAC and PLL



# Summary

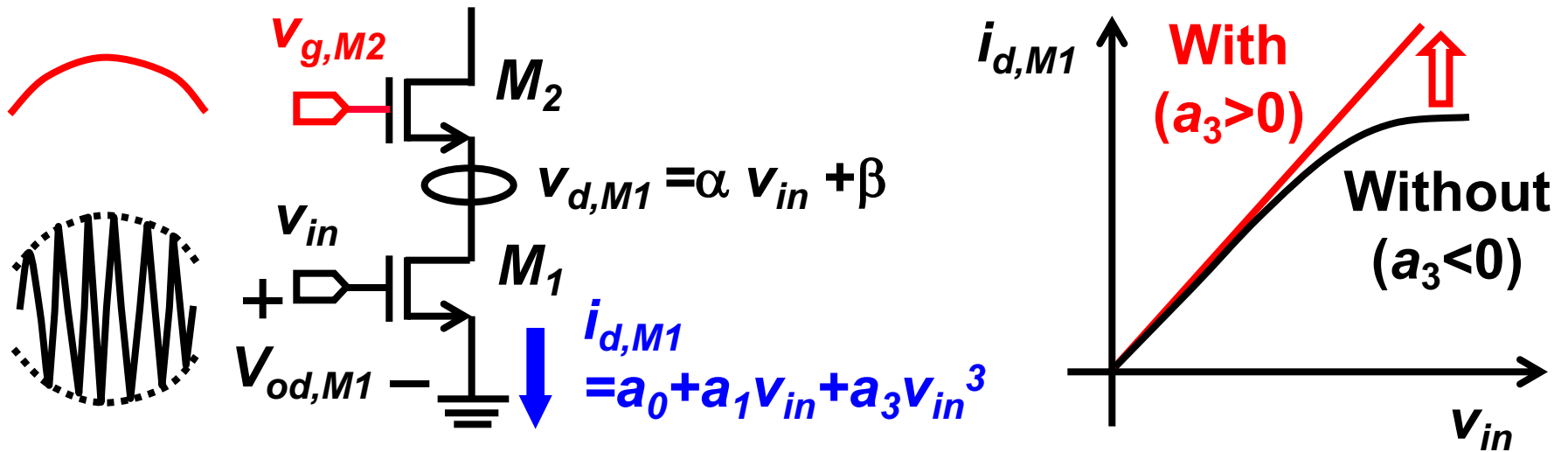
Multiband LTE SAW-less transmitter demonstrated:

- **Source-follower-driven passive mixer**
  - Reduces chip area ( $0.2 \text{ mm}^2$ ) and power consumption (13 mW)
- **Envelope-tracked basing for RF-PGA**
  - Improves ACLR by 3 dB
- **Marchand balun**
  - Provides less loss and broader 1-dB bandwidth than transformer
- ACLR  $< -42 \text{ dBc}$ , EVM  $< 3\%$ , and RX-band noise  $< -158 \text{ dBc/Hz}$  from 700 MHz to 2.6 GHz





# Envelope-Tracked Biasing



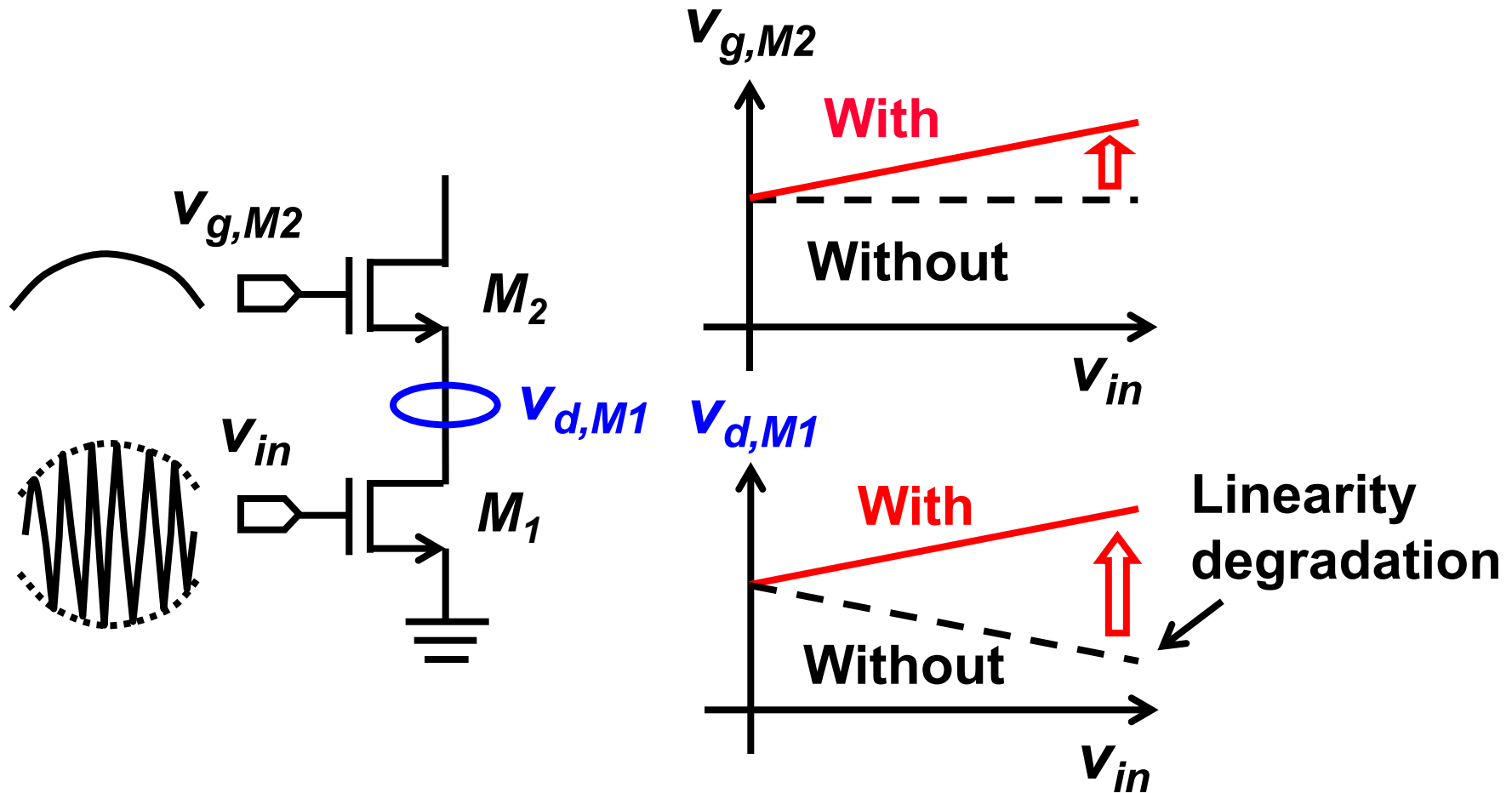
	With	Without
$\frac{a_1}{a_3}$	$V_{od,M1}^2 + \frac{1}{\alpha} \left( 2\beta + \frac{2}{\lambda} \right) V_{od,M1}$	$V_{od,M1}^2 - \left( 2\beta + \frac{2}{\lambda} \right) V_{od,M1}$

$\lambda$ : Channel-length modulation coefficient

The gate voltage of M2 ( $v_{g,M2}$ ) tracks to envelope signal and the linearity of transconductor improves



# Envelope-Tracked Biasing (1)



The gate voltage of  $M_2$  ( $v_{g,M2}$ ) tracks envelope signal and the linearity of transconductor improves

